

### Webinar: Part 2 – Equipment Testing Advanced Method for Compaction Quality Control

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Webinar Moderator



### **Professional**

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## Housekeeping

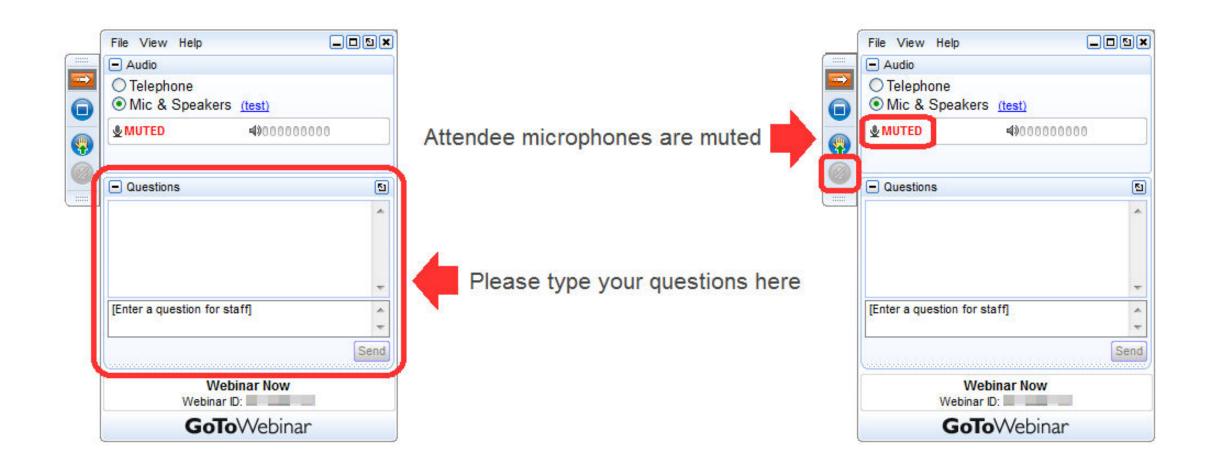


Webinar 60 mins Questions 10 mins





### **GoTo Webinar functions**







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Part 1 – An Overview (Conceptual)

- ✓ Density Basics
- ✓ Rationale for this equipment research
- ✓ Equipment overview + a few initial findings

Part 2 – Test Results **(Technical)** 

- Details of testing from various sites
- Correlations with "Standard" practice
- Time vs Reliability vs Useful Data

2018 Presentation 2020 Presentations



Part 3 – Moving Forward (**Procedural**)

- Procedures and Specifications
- Advantages and limitations
- Implementation



P60: Best practice in compaction quality assurance for subgrade materials

ARRB Project Leader: Dr. Jeffrey Lee

TMR Project Manager: Siva Sivakumar

http://nacoe.com.au/





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### NACOE P60

Aim and Background of the Project

- Aim
  - To modernise testing procedure for compaction quality assurance
- Background
  - Quality is conventionally been verified using density measurements
  - Alternative methods have been developed over the past two decades
  - Many of these methods takes less time to do, results become available in a much shorter time frame, and is able to measure in situ stiffness.





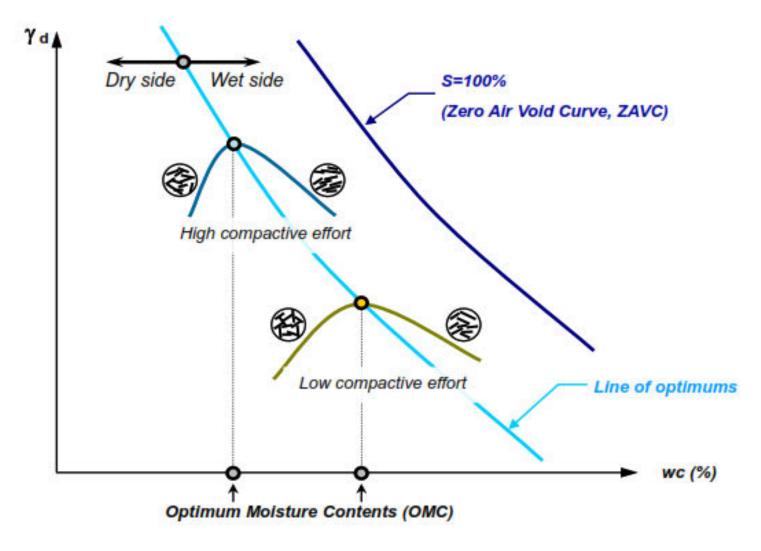


## Compaction Basics In 5 slides

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### Target low air voids $\rightarrow$ Line of optimums

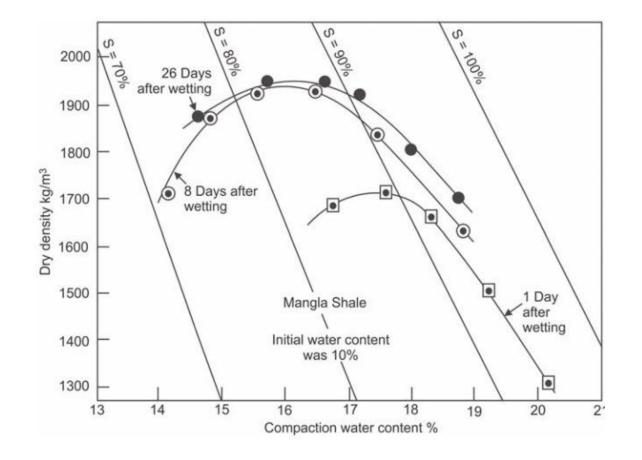




Examples of compaction curves (modified after Lambe 1962).



### Sampling Curing is required



### TABLE 4

#### MINIMUM CURING TIME

| District                     | Condition of prepared sample |                          |  |  |  |  |  |
|------------------------------|------------------------------|--------------------------|--|--|--|--|--|
| Plasticity                   | Within 2% of OMC             | Greater than 2% from OMC |  |  |  |  |  |
| Sands and granular material* | 2 h                          | 2 h                      |  |  |  |  |  |
| Low ( <i>LL</i> ≤35%)        | 24 h                         | 48 h                     |  |  |  |  |  |
| Medium (35% < LL ≤50%)       | 48 h                         | 96 h (4 days)            |  |  |  |  |  |
| High $(LL > 50\%)$           | 96 h (4 days)                | 168 h (7 days)           |  |  |  |  |  |

\* These can include naturally occurring sands and gravels, crushed rocks and manufactured materials with fines content typically less than 12%.

LEGEND:

LL - liquid limit

OMC - optimum moisture content

| Australian | Standard <sup>®</sup> |
|------------|-----------------------|
|------------|-----------------------|

Methods of testing soils for engineering purposes Method 5.1.1: Soil compaction and density tests—Determination of the dry density/moisture content relation of a soil using standard compactive effort

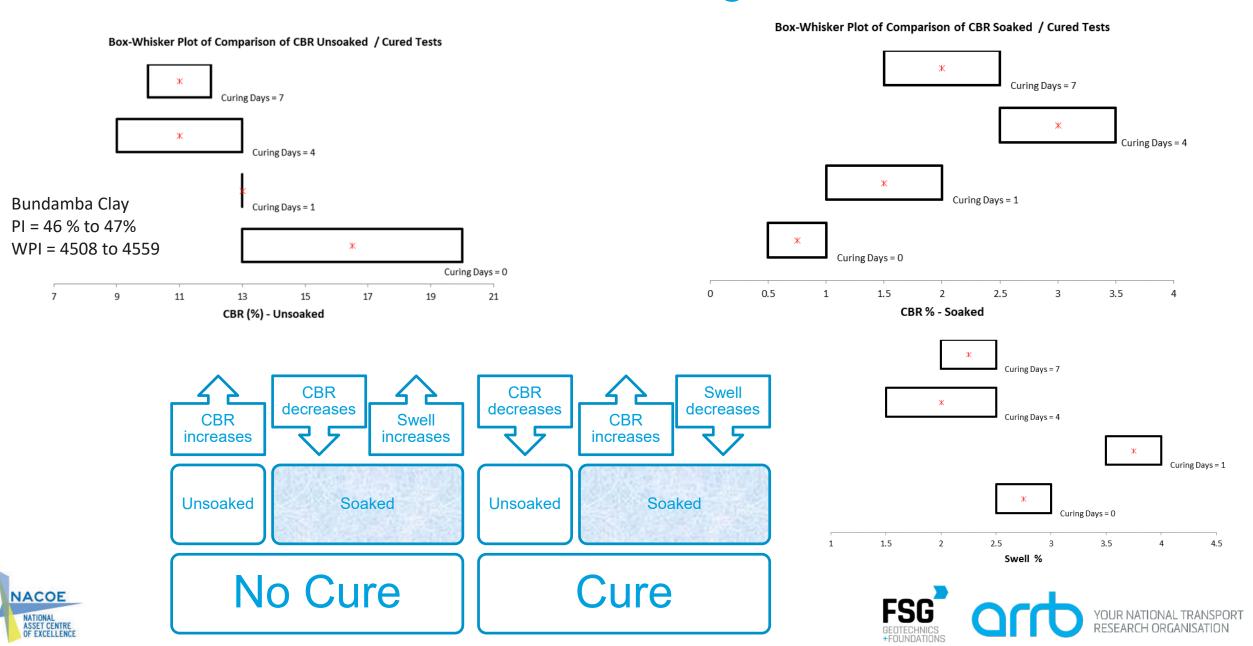




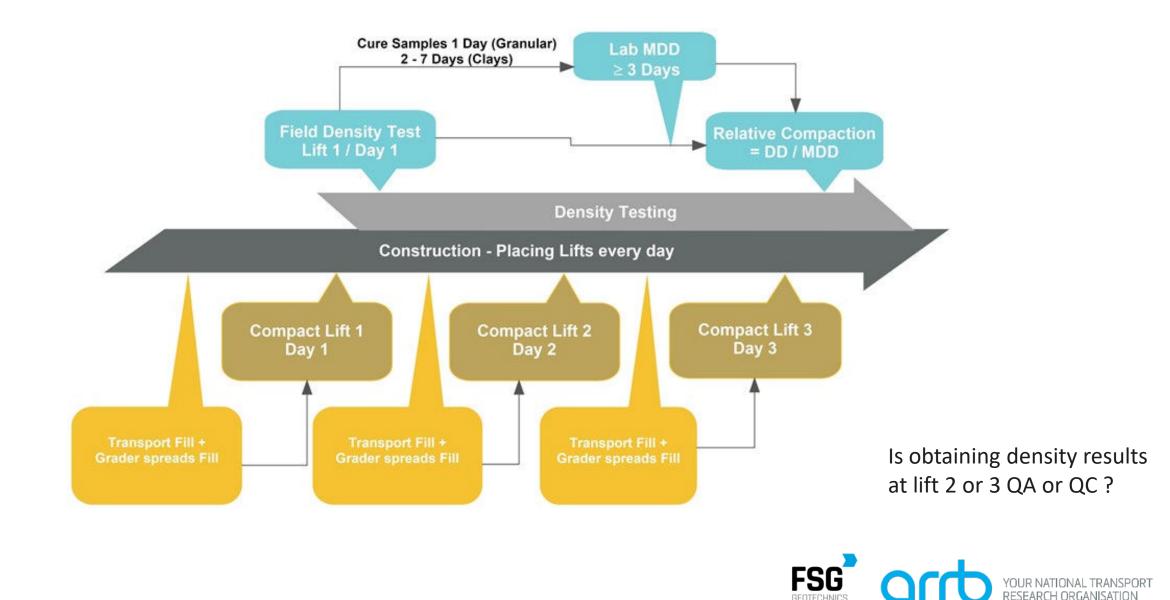
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### Unsoaked + CBR – Effect of curing

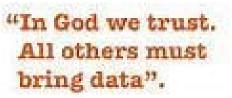


### Density Ratio compaction tests are lag indicators





14



W. Edwards Deming

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# What does Quality look like ?





QA is *process* oriented (verification) vs QC is *product* oriented (validation).

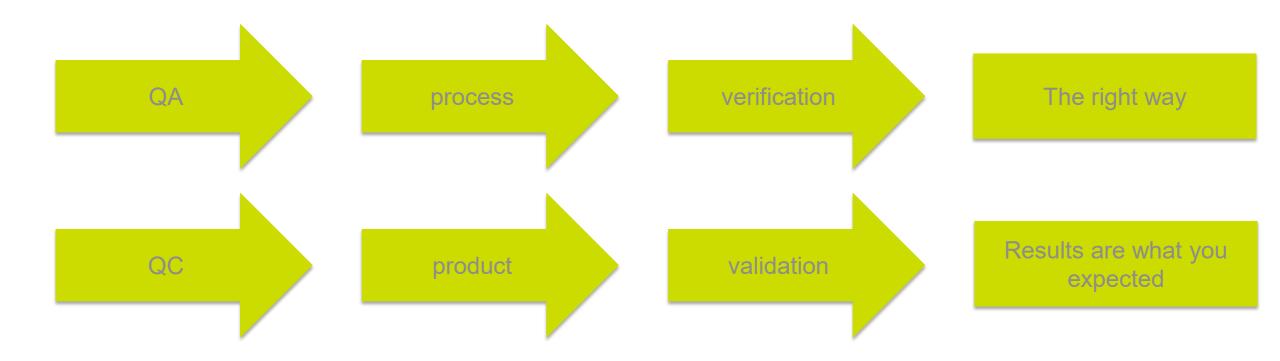
QA aims to prevent defects. QC aims to identify and fix defects

- Quality Assurance makes sure you are doing the right things, the right way
- Quality **Control** makes sure the results of what you've done are what you expected.





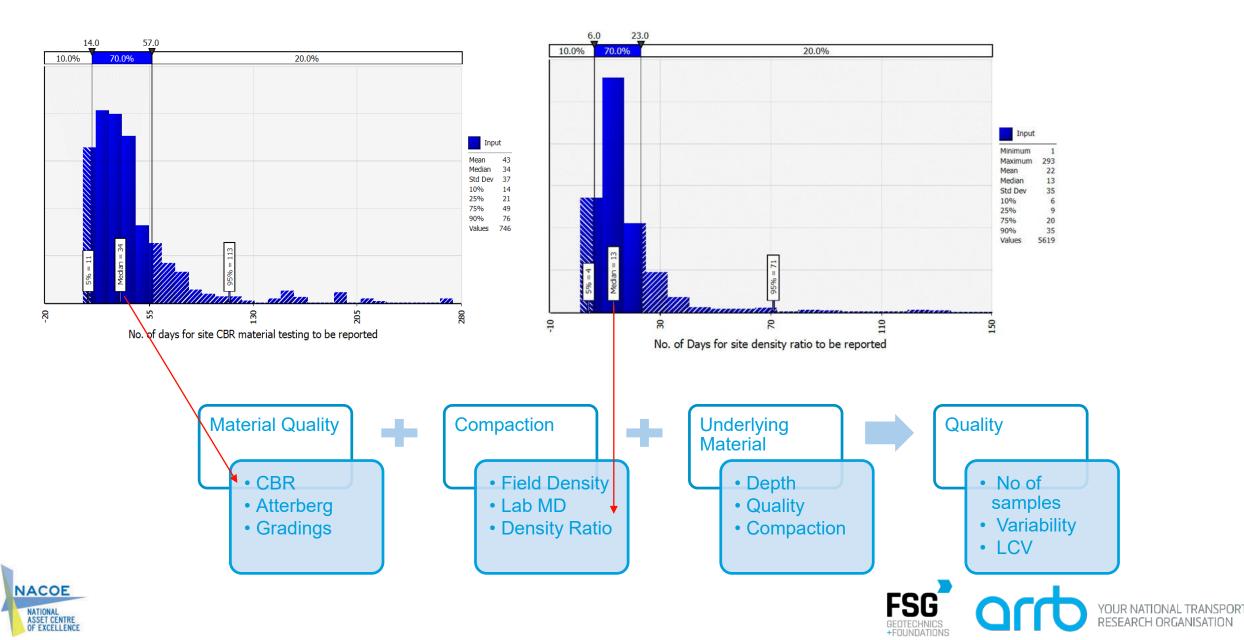
### Quality Control (QC) vs Quality Assurance (QA)



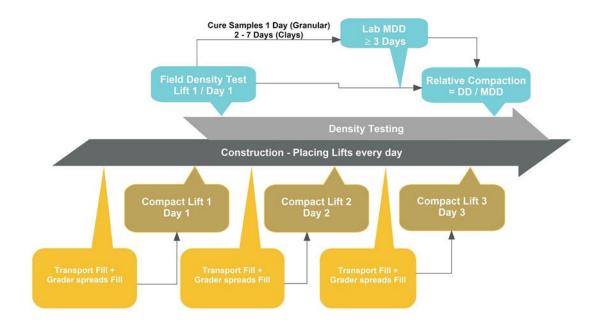


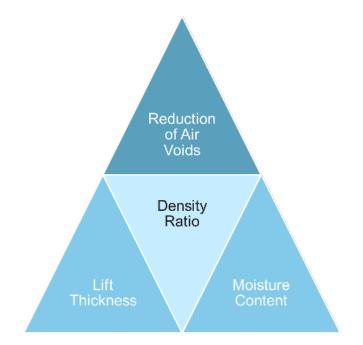


### Construction records – Quality tests reporting



### Density Ratio tests – Objectives + Process





Many contractors, often place additional lifts before the test results are known / reported.

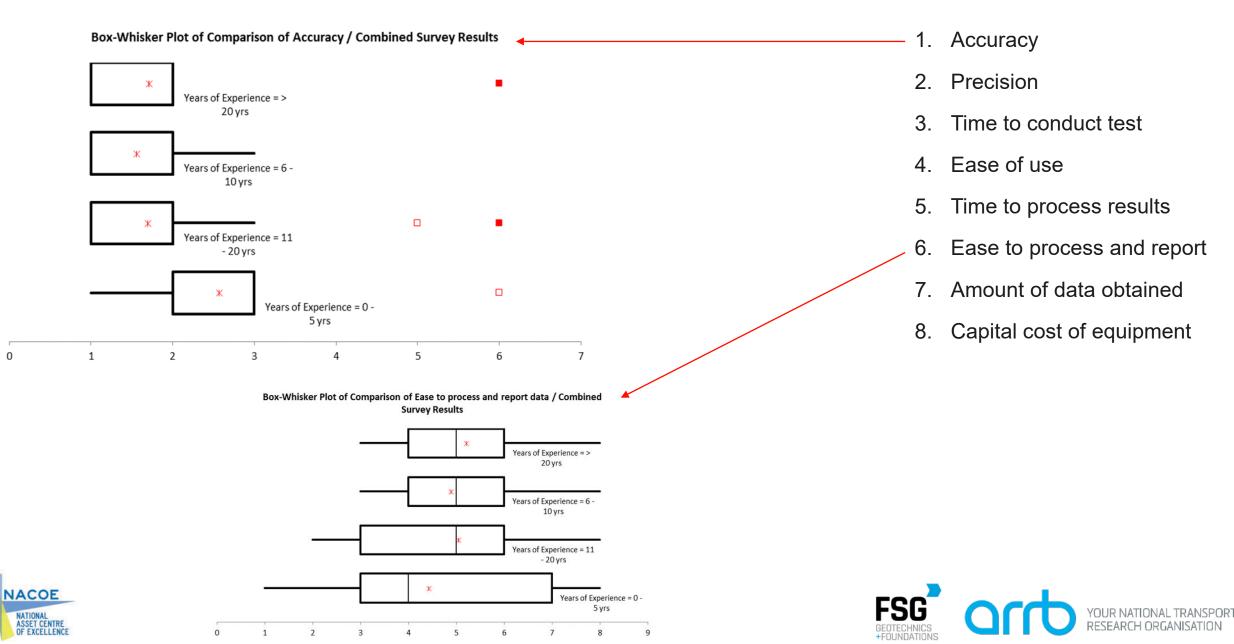
This has a risk, but is based on the assumption that they have achieved compaction and the tests are simply validating (QC) what they already known based on

- $\checkmark$  No. of passes
- ✓ Lift Thickness
- ✓ Moisture Content





### What do Engineers want



### Preference Ranking based on years of experience

| Rank |                               | 0 - 5 yrs              | 6 - 10 yrs             | 11 - 20 yrs                | > 20 yrs                   |  |  |
|------|-------------------------------|------------------------|------------------------|----------------------------|----------------------------|--|--|
|      | No in Sample                  | 7                      | 9                      | 23                         | 15                         |  |  |
| 1.   | Accuracy                      | No. 2/3                | No. 1 / 2              | No. 1 / 2                  | Narrow Band<br>No. 1 / 2   |  |  |
| 2.   | Precision                     | No. 3                  | Wide Band<br>No. 3     | Wide Band<br>No. 3 / 4 / 5 | Narrow Band<br>No. 2       |  |  |
| 3.   | Time to conduct test          | Wide Band<br>No. 4 / 5 | Wide Band<br>No. 5     | Wide Band<br>No. 3 / 4     | Wide Band<br>No. 4 / 5 / 6 |  |  |
| 4.   | Ease of use                   | Wide Band<br>No. 4     | Wide Band<br>No. 5     | Wide Band<br>No.5          | Wide Band<br>No. 4         |  |  |
| 5.   | Time to process<br>results    | Wide Band<br>No. 4 / 5 | Wide Band<br>No. 4 / 5 | Wide Band<br>No. 3 / 4     | Wide Band<br>No. 5         |  |  |
| 6.   | Ease to process<br>and report | Wide Band<br>No. 4     | No. 5                  | No. 5                      | No.5                       |  |  |
| 7.   | Amount of data<br>obtained    | Narrow band<br>No. 7   | Wide Band<br>No. 6     | Wide Band<br>No. 5         | Wide Band<br>No. 5         |  |  |
| 8.   | Capital cost of equipment     | No. 7                  | Wide Band<br>No. 6 /7  | Wide Band<br>No. 5 / 7     | Narrow band<br>No. 7       |  |  |

A survey of 54 engineers ranked what attributes are desirable in a test equipment

Attributes were ranked

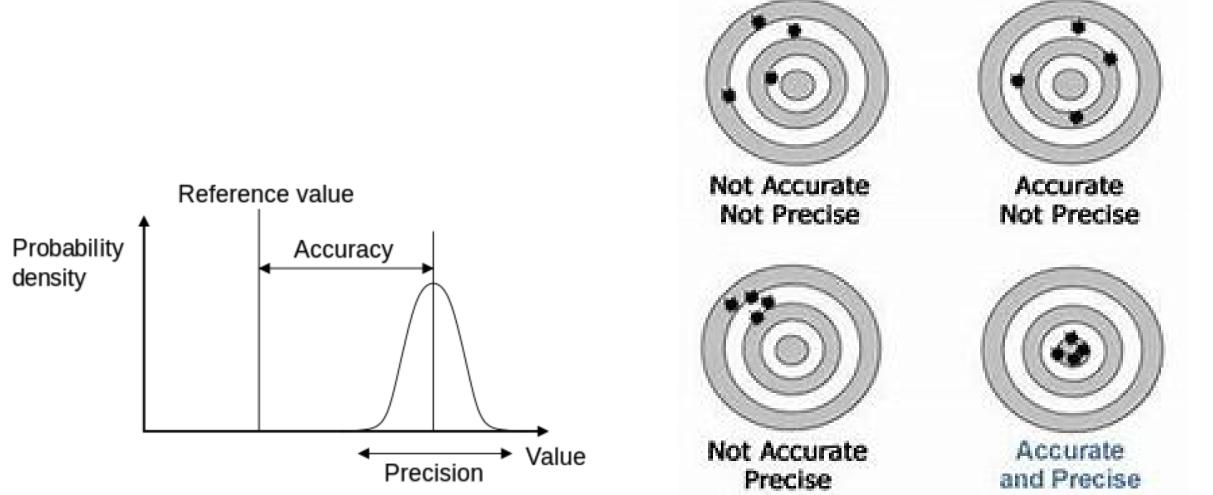
### 1. Accuracy

Accuracy refers to closeness of the measurements to a "true" value, while precision refers to the closeness of the measurements to each other (repeatability).





### Accuracy vs Precision







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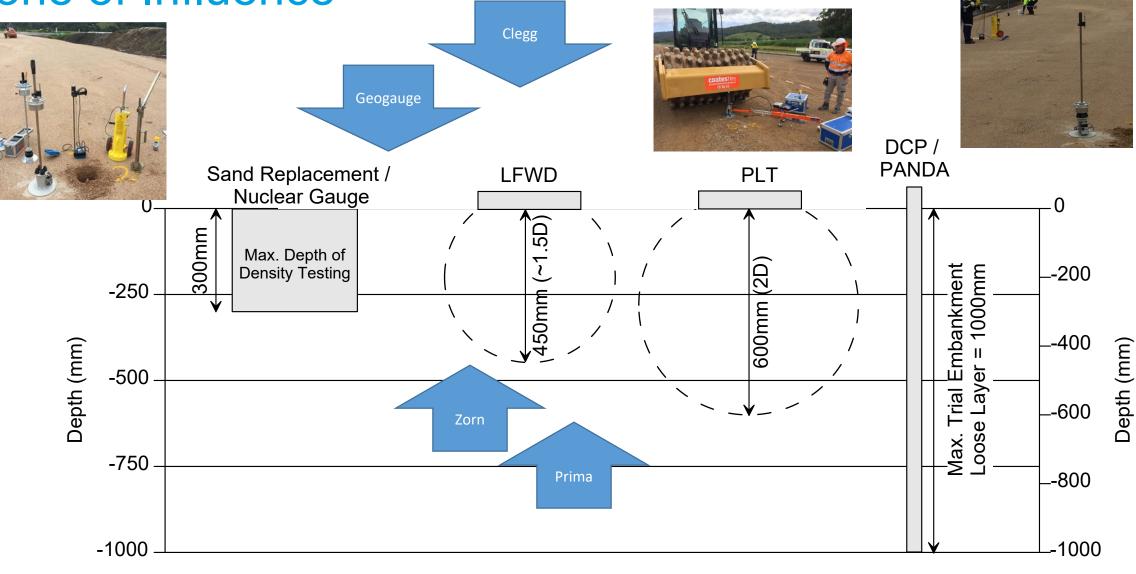


## Comparison of Test Equipment





### Zone of Influence







Testing

### **Clegg** Hammer



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### LFWD - Blue Tooth Connectivity



### Plate Load Test





### Intelligent Compaction - Testing with roller



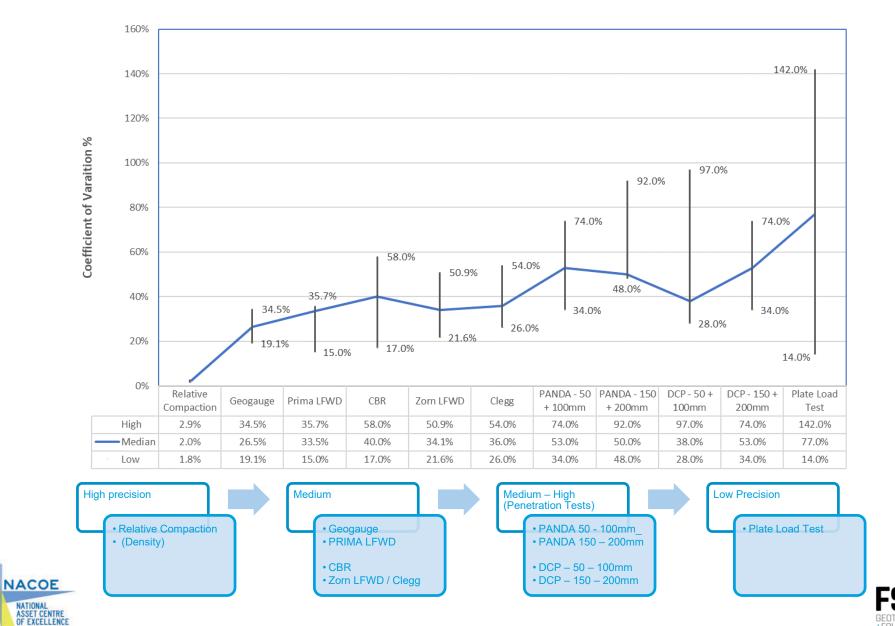
### CMV – Compaction Meter Value







### **Equipment Precision**



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### Equipment matches to other tests (5 sites)

| Accuracy                | PLT | Density | Geogauge | LFWD -<br>ZORN | LFWD -<br>PRIMA | Clegg | PANDA -<br>100mm | PANDA -<br>200mm | DCP 100mm | DCP 200mm | CBR | Moisture<br>Ratio |
|-------------------------|-----|---------|----------|----------------|-----------------|-------|------------------|------------------|-----------|-----------|-----|-------------------|
| PLT                     |     | 1       | 0        | 0              | 3               | 3     | 4                | 2                | 0         | 5         | 3   | 1                 |
| Density                 | 1   |         | 0        | 1              | 1               | 1     | 1                | 2                | 0         | 4         | 1   | 1                 |
| Geogauge                | 0   | 0       |          | 3              | 5               | 0     | 0                | 0                | 2         | 0         | 0   | 1                 |
| LFWD - ZORN             | 0   | 1       | 3        |                | 3               | 0     | 0                | 1                | 2         | 0         | 0   | 1                 |
| LFWD - PRIMA            | 3   | 1       | 5        | 3              |                 | 0     | 0                | 0                | 2         | 1         | 0   | 1                 |
| Clegg                   | 3   | 1       | 0        | 0              | 0               |       | 3                | 3                | 2         | 0         | 3   | 0                 |
| PANDA -50/100mm         | 4   | 1       | 0        | 0              | 0               | 3     |                  | 3                | 0         | 2         | 5   | 1                 |
| PANDA -150/200mm        | 2   | 2       | 0        | 1              | 0               | 3     | 3                |                  | 1         | 1         | 3   | 1                 |
| DCP 50/100mm            | 0   | 0       | 2        | 2              | 2               | 2     | 0                | 1                |           | 0         | 0   | 0                 |
| DCP 150/200mm           | 5   | 4       | 0        | 0              | 1               | 0     | 2                | 1                | 0         |           | 1   | 1                 |
| CBR                     | 3   | 1       | 0        | 0              | 0               | 3     | 5                | 3                | 0         | 1         |     | 1                 |
| Moisture Ratio          | 1   | 1       | 1        | 1              | 1               | 0     | 1                | 1                | 0         | 1         | 1   |                   |
|                         |     |         |          |                |                 |       |                  |                  |           |           |     |                   |
| No. of Matches          | 22  | 13      | 11       | 11             | 16              | 15    | 19               | 17               | 9         | 15        | 17  | 9                 |
| Rank ito cross matching | 1   | 8       | 9        | 9              | 5               | 6     | 2                | 3                | 11        | 6         | 3   | 11                |

HighMedianLow

Sites compared for 5 sites tested

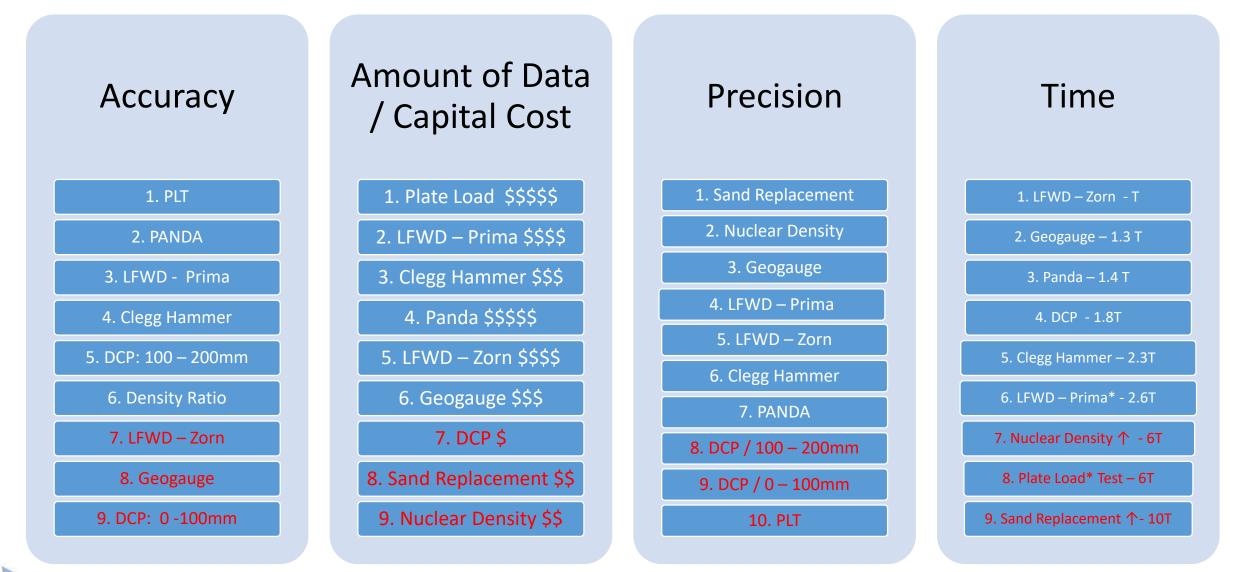
No. of matches used as an indicator of accuracy

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### Summary of some field test equipment attributes





\* Complete Stress Strain response provided – not provided by other equipment ↑ Larger Reporting time. Moisture or air voids may be determined

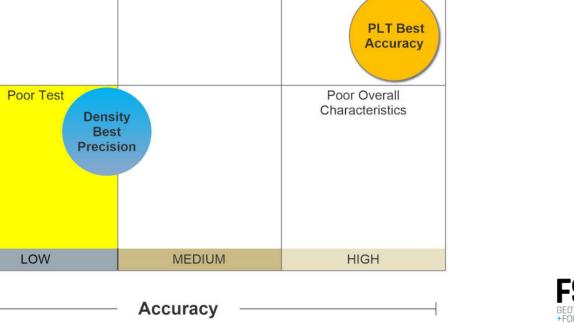
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### What industry wants and equipment position

#### Poor Accuracy Ideal Test H Precision + G + H Time to do Amount of Data + Capital Cost PANDA, CLEGG, Ease GEOGAUGE, DCP, LFWD (Prima + Zorn) test + M of Use Е D Time to report Test + U **PLT Best** ÷ M Accuracy Ease to Process Poor Overall Poor Test Characteristics Density Best Precision 0 W Data

**Accuracy vs Other Equipment Characteristics** 







## 'ALTERNATIVE FACTS'

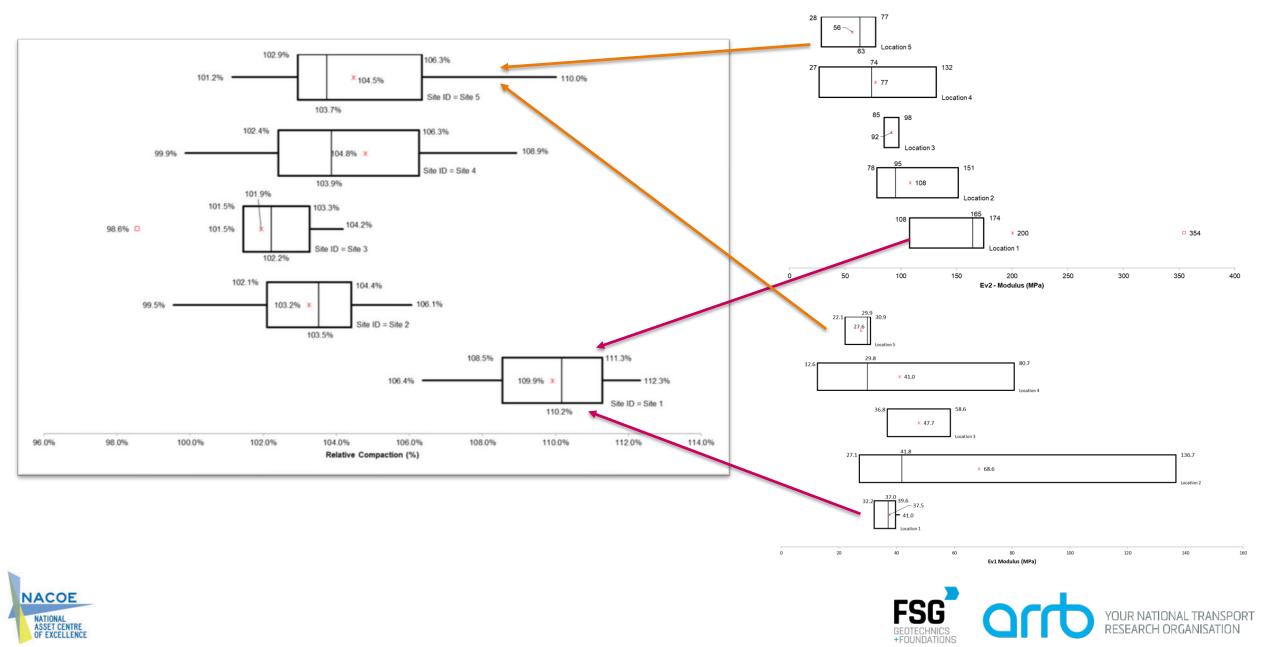
### WHEN YOU CAN'T HANDLE THE TRUTH

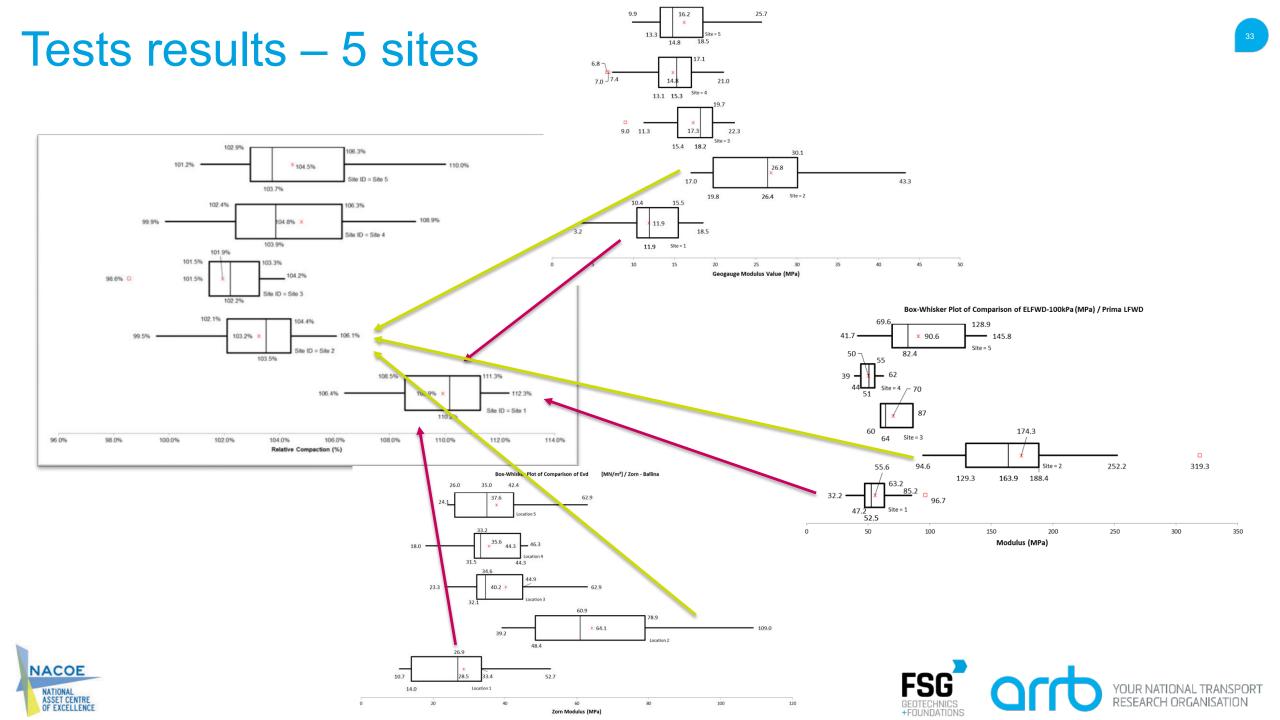
## Alternative Equipment / Testing



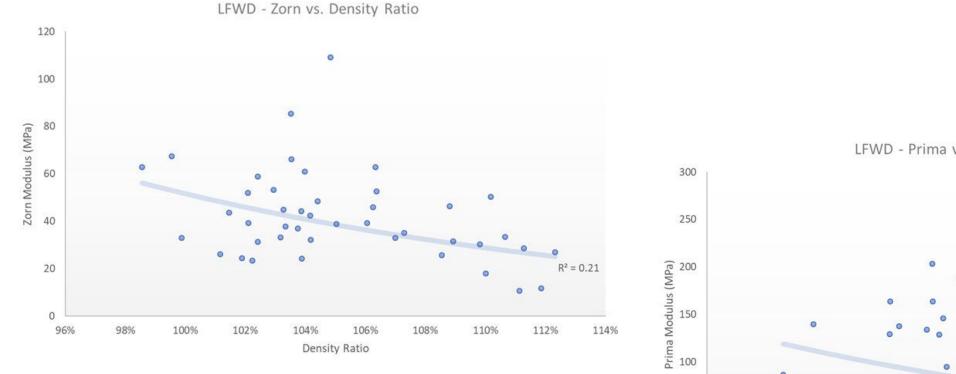


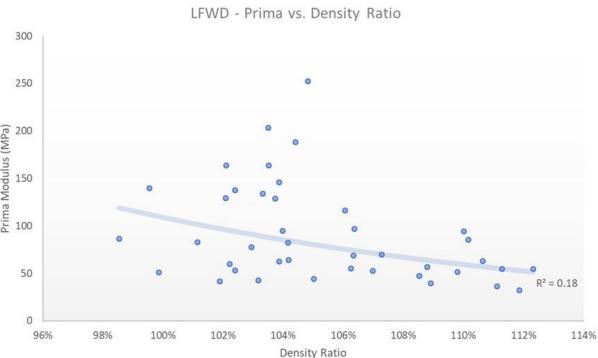
### Tests results – 5 sites





### LFWD (Zorn + Prima) correlated to density ratio

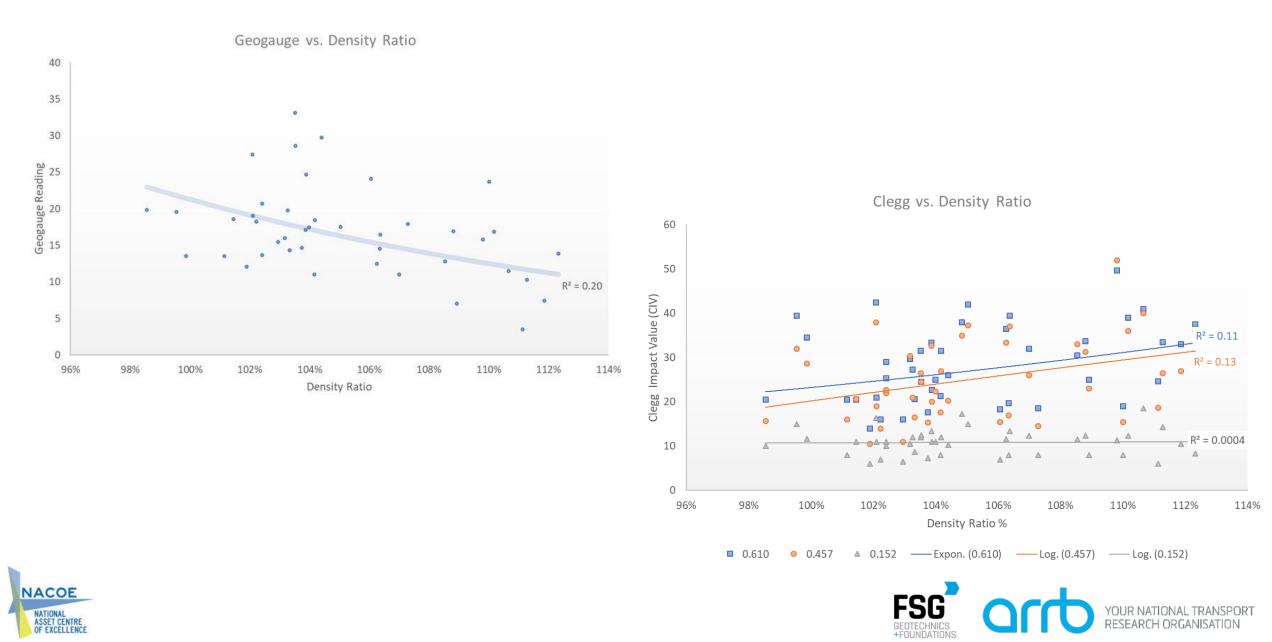








### Geogauge and Clegg correlated to density ratio



### **Paired Correlations**

Some base assumptions made

- As density ratio increases the CBR, modulus, or strength increases
- A suitable trend line would be apparent may not necessarily be linear
- Relative Compaction (Density ratio) as the well-established measurement would be correct (accurate)

Density Ratio compared with modulus measured with 2 different LFWD (ZORN + PRIMA) + CLEGG + GEOGAUGE

- $\circ~$  Low correlation (R<sup>2</sup> ~ 0.2) shows such relationships should not be used
- More importantly as density ratio increased, all alternate tests decreased. Suggests that as compacted density increases to high values the modulus decreases. This is counter intuitive.
- Results for this data show common assumption that  $\uparrow$  DR $\rightarrow$   $\uparrow$  modulus may be incorrect.











Measurement Shift

## CLOSE ENOUGH

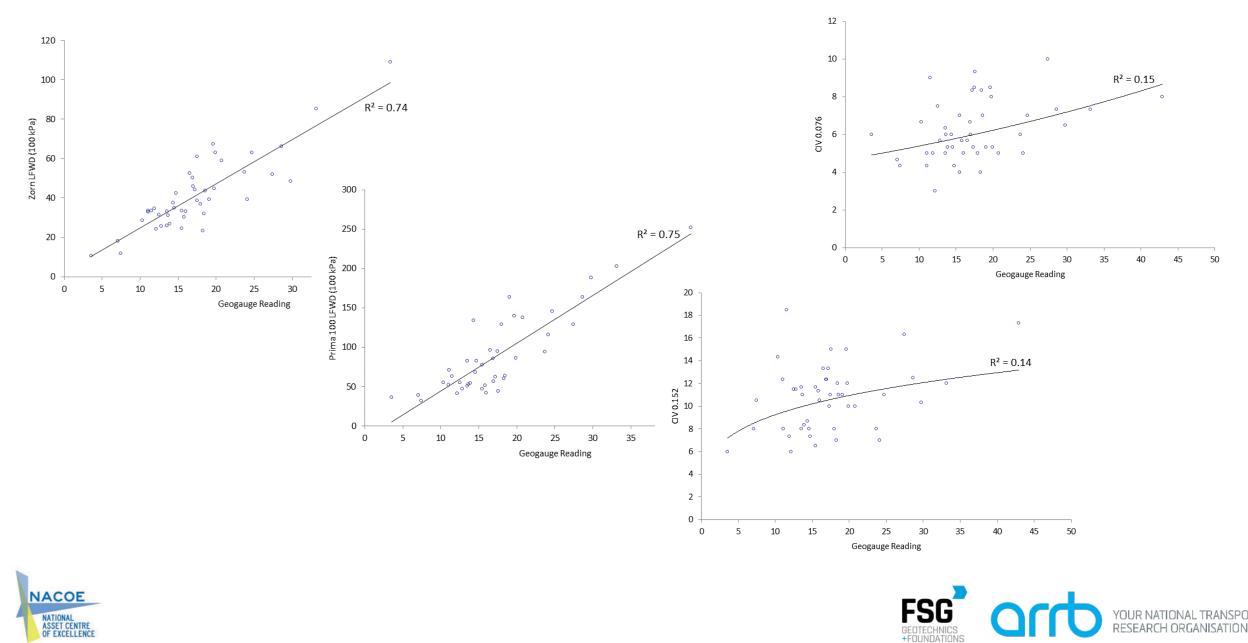
http://favoritememes.com/news/close\_enough/2014-07-27-342

# Alternative Equipment / Testing





#### But Alternate Tests correlate to each other

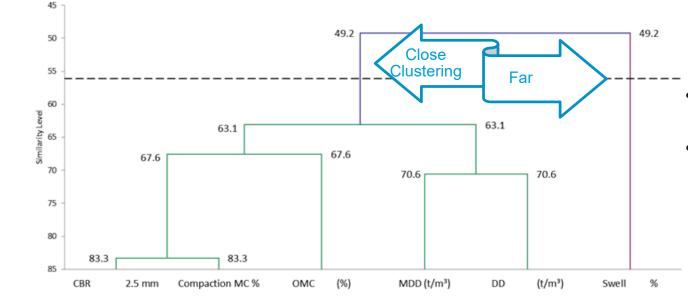


### **Dendogram Analysis**

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- In statistics, hierarchical clustering builds cluster trees (Dendograms) to represent clustered data.
- Groups of data are nested and organized as a tree with each group in liking to other successor groups.
   StatTools (version 7) an add-in to Microsoft Excel was used for this cluster analysis.
- The Cluster Analysis command searches for patterns in a data set → classify observations or variables into groups of similar items. Analysis supports a variety of agglomerative hierarchical methods and distance measures. The *clade* is a branch in the tree. Clades that are close to the same height are similar to each other and clades with different heights are dissimilar. Greater distance in height the more dissimilarity



• Dendogram for Cooroy (CH) clay Soaked CBR.

Clustering provides visual evidence that CBR is more closely clustered to compaction moisture and the OMC rather than the density.



### Dendogram vs correlation matrix (6 variables)

- CBR most strongly correlated with compaction MC (0.691) •
- •
- Least with the MDD (-0.04) CBR negatively correlated with swell (-0.834). •

| CBR negatively contenated with swell (-0.834).   | Correlation<br>Matrix   | Comp<br>MC % | DD<br>(t/m³) | OMC<br>(%) | MDD<br>(t/m³) | CBR<br>@ 2.5mm | Swell<br>% |
|--|-------------------------|--------------|--------------|------------|---------------|----------------|------------|
| 45 Close<br>Clustering<br>Far  | Comp. MC %              | 1.00         |              |            |               |                |            |
| 49.2 49.2 49.2 55  | DD (t/m <sup>3</sup> )  | -0.30        | 1.00         |            |               |                |            |
| 63.1<br>63.1<br>63.1<br>63.1<br>63.1<br>63.1<br>63.1<br>63.1<br>63.1<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70 | OMC (%)                 | 0.23         | -0.38        | 1.00       |               |                |            |
| 80 - 83.3 83.3   | MDD (t/m <sup>3</sup> ) | -0.04        | 0.46         | -0.34      | 1.00          |                |            |
| x, 05.5 05.5 05.5 05.5 05.5 05.5 05.5 05.  | CBR<br>@2.5 mm          | 0.69         | 0.04         | 0.40       | 0.32          | 1.00           |            |
|  | Swell %                 | -0.85        | 0.06         | -0.14      | -0.38         | -0.83          | 1.00       |





#### **Correlation Matrix Soaked CBR**

| Corr   | elation             | Compaction<br>MC % | DD<br>(t/m³) | OMC (%) | MDD (t/m³) | OVMC (%) | CBR<br>2.5 mm | CBR<br>5 mm | Swell % | Avg MC after<br>soak | DD (t/m³)<br>after soak | MC Top Layer<br>(%) AP | Avg MC<br>(%) AP | δGMC | (%)   |
|--------|---------------------|--------------------|--------------|---------|------------|----------|---------------|-------------|---------|----------------------|-------------------------|------------------------|------------------|------|-------|
| Compac | tion MC %           | 1.00               | . ,          |         |            |          |               |             |         |                      |                         |                        |                  |      |       |
| DD     | (t/m³)              | -0.84              | 1.00         | )       |            |          |               |             |         |                      |                         |                        |                  |      |       |
| OMC    | (%)                 | 0.84               | -0.89        |         |            |          |               |             |         |                      |                         |                        |                  |      |       |
|        | ) (t/m³)            | -0.88              | 0.97         |         |            |          |               |             |         |                      |                         |                        |                  |      |       |
|        | 1C (%)              | 0.82               | -0.84        | 0.98    | -0.86      | 1.00     |               |             |         |                      |                         |                        |                  |      |       |
| CBR    | 2.5 mm              | -0.47              | 0.61         | -0.49   | 0.59       | -0.47    | 1.00          |             |         |                      |                         |                        |                  |      |       |
| CBR    | 5 mm                | -0.56              | 0.66         |         |            |          | 0.90          | 1.00        |         |                      |                         |                        |                  |      |       |
| Swell  | %                   | 0.41               | -0.62        |         |            |          | -0.79         | -0.75       |         |                      |                         |                        |                  |      |       |
|        | after soak          | 0.43               | -0.84        |         |            |          | -0.61         | -0.65       |         |                      |                         |                        |                  |      |       |
|        | ) after soak        | 0.39               | 0.20         | -0.04   | 0.22       | 0.13     | 0.53          | 0.52        | -0.58   | -0.68                | 1.00                    |                        |                  |      |       |
|        | ayer (%) AP         | 0.33               | -0.71        |         |            |          | -0.71         | -0.76       |         |                      | -0.76                   |                        |                  |      |       |
| Avg MC | (%) AP              | 0.55               | -0.89        |         |            |          | -0.64         | -0.69       |         |                      | -0.67                   |                        | 1.00             |      |       |
| δGMC   | . ,                 | -0.24              | -0.23        |         |            |          | -0.84         | -0.86       |         |                      |                         |                        | 0.56             |      | 1.00  |
|        | (t/m <sup>3</sup> ) | -0.77              | 0.45         |         |            |          | -0.60         | -0.60       |         |                      |                         |                        | 0.21             |      | 0.78  |
|        | at Comp.            | 0.96               | -0.72        |         |            |          | -0.39         | -0.49       |         |                      | 0.45                    |                        | 0.41             |      | -0.35 |
|        | fter soak           | 0.18               | -0.71        |         |            |          | -0.29         | -0.26       |         |                      |                         |                        | 0.86             |      | 0.17  |
|        | /MC                 | -0.85              | 0.13         |         |            |          | -0.91         | -0.89       |         |                      | -0.51                   |                        | 0.47             |      | 0.97  |
| MR a   | it comp             | 0.42               | -0.05        |         |            |          | 0.03          | -0.08       | -0.34   | -0.27                | 0.48                    |                        | -0.21            |      | -0.64 |
| MR s   | soaked              | -0.02              | -0.19        | -0.11   | -0.11      | -0.18    | -0.76         | -0.73       | 0.68    | 0.50                 | -0.53                   | 0.57                   | 0.47             |      | 0.66  |
| DR a   | t Comp              | 0.01               | 0.27         | -0.04   | 0.05       | -0.06    | 0.18          | 0.11        | -0.05   | -0.29                | 0.14                    | -0.13                  | -0.33            |      | 0.05  |
| Dr s   | oaked               | 0.64               | -0.17        | 0.36    | -0.28      | 0.39     | 0.56          | 0.55        | -0.59   | -0.36                | 0.85                    | -0.53                  | -0.35            |      | -0.66 |
| VMC    | at comp             | 0.40               | -0.01        | -0.07   | -0.05      | -0.10    | 0.01          | -0.10       | -0.30   | -0.29                | 0.46                    | -0.34                  | -0.23            |      | -0.63 |
| VMR    | soaked              | -0.29              | 0.01         | -0.47   | 0.13       | -0.65    | -0.51         | -0.47       | 0.44    | 0.49                 | -0.24                   | 0.52                   | 0.50             |      | 0.44  |
| Gs as  | ssumed              | 0.00               | 0.00         | 0.00    | 0.00       | 0.00     | 0.00          | 0.00        | 0.00    | 0.00                 | 0.00                    | 0.00                   | 0.00             |      | 0.00  |
|        | erpreted            | -0.03              | 0.13         | 3 0.07  | 0.12       | 0.16     | 0.03          | 0.11        | 0.03    | 0.55                 | 0.14                    | 0.47                   | 0.64             |      | 0.14  |
|        | efore               | 0.74               | -1.00        |         |            |          | -0.38         | -0.45       |         |                      | -0.20                   |                        | 0.87             |      | 0.23  |
|        | after               | -0.39              | -0.20        |         |            |          | -0.53         | -0.52       |         |                      | -1.00                   |                        |                  |      | 0.60  |
|        | pefore              | -0.69              | 0.16         |         |            |          | -0.55         | -0.52       |         |                      |                         |                        | 0.11             |      | 0.76  |
|        | after               | -0.59              | 0.37         |         |            |          | -0.31         | -0.33       |         |                      |                         |                        |                  |      | 0.44  |
|        | Av                  | -0.62              | -0.15        |         |            |          | -0.81         | -0.78       |         |                      | -0.35                   |                        | 0.56             |      | 0.78  |
|        | efore               | 0.74               | -1.00        |         |            |          | -0.38         | -0.45       |         |                      | -0.20                   |                        | 0.87             |      | 0.23  |
|        | after               | -0.39              | -0.20        |         |            |          | -0.53         | -0.52       |         |                      | -1.00                   |                        | 0.67             |      | 0.60  |
|        | δn                  | -0.77              | 0.45         |         |            |          | -0.60         | -0.60       |         |                      |                         |                        | 0.21             |      | 0.78  |
|        | before              | 0.79               | -0.27        |         |            |          | 0.45          | 0.41        | -0.39   |                      | 0.51                    |                        |                  |      | -0.68 |
|        | S after             | 0.58               | -0.40        |         |            |          | 0.28          | 0.30        |         |                      |                         |                        |                  |      | -0.42 |
| δΙ     | DOS                 | -0.68              | -0.08        | -0.04   | -0.04      | -0.12    | -0.84         | -0.81       | 0.66    | 0.54                 | -0.36                   | 0.58                   | 0.53             |      | 0.82  |





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| Correlation Matrix Soaked CBR                | CBR         5 mm           CBR         2.5 mm           δ VMC           δ GMC         (%)           δ DOS           δ Av | mm<br>0.898<br>1.000<br>-0.912<br>-0.843 | mm<br><u>1.000</u><br><u>0.898</u><br>-0.889<br>-0.858 |
|--|--|--|--|
| 2<br>3                                       | CBR         2.5 mm           δ VMC           δ GMC         (%)           δ DOS   | 1.000<br>-0.912<br>-0.843                | 0.898<br>-0.889  |
| 3  | δ VMC<br>δ GMC (%)<br>δ DOS  | -0.912<br>-0.843                         | -0.889   |
|  | δ GMC (%)<br>δ DOS   | -0.843                                   |  |
| 4  | δDOS   |  |  |
| 5  |  |  | -0.810   |
|  |  | -0.838<br>-0.814                         | -0.783   |
| CBR ~ Modulus                                | MC Top Layer (%) AP  | -0.706                                   | -0.759   |
|  | Swell %  | -0.787                                   | -0.754   |
| 9  | MR soaked  | -0.762                                   | -0.728   |
| • > 0.80                                     | Avg MC (%) AP  | -0.637                                   | -0.688   |
|  | MDD (t/m <sup>3</sup> )  | 0.589                                    | 0.662  |
| • VMC / GMC                                  | DD (t/m <sup>3</sup> )   | 0.606                                    | 0.661  |
|  | Avg MC after soak  | -0.608                                   | -0.652   |
| • $\delta$ DOS / $\delta$ Air Voids          | δn   | -0.602                                   | -0.604   |
| 15   | δDD (t/m³)   | -0.602                                   | -0.604   |
| 16   | Compaction MC %  | -0.471                                   | -0.564   |
| 17   | Dr soaked  | 0.558                                    | 0.552  |
| 18   | DD (t/m³) after soak   | 0.529                                    | 0.520  |
|  | n after  | -0.529                                   | -0.520   |
| DR 0.18 / 0.11 ~ 20                          | e after  | -0.529                                   | -0.520   |
| 21   | Av before  | -0.548                                   | -0.517   |
|  | VMC at Comp.   | -0.391                                   | -0.488   |
| $\sim$ MR 0.03 / -0.08 $\sim$ 22<br>23       | OMC (%)  | -0.488                                   | -0.488   |
| 24   | VMR soaked   | -0.511                                   | -0.471   |
|  | OVMC (%)   | -0.465                                   | -0.460   |
| 26   | n before   | -0.382                                   | -0.449   |
| 27   | e before   | -0.382                                   | -0.449   |
| 28   | DOS before   | 0.446                                    | 0.408  |
| 29   | Av after   | -0.309                                   | -0.326   |
| 30   | DOS after  | 0.280                                    | 0.298  |
| From 36 variables in a CBR test              | VMC after soak   | -0.286                                   | -0.256   |
| 32   | DR at Comp   | 0.185                                    | 0.111  |
| Construction focuses on DR and MR            | Gs Interpreted   | 0.026                                    | 0.109  |
|  | VMC at comp  | 0.009                                    | -0.099   |
| which are poorly correlated to CBR (Modulus) | MR at comp   | 0.026                                    | -0.081   |
| 36   | Gs assumed   | 0.000                                    | 0.000  |
| NATIONAL<br>ASSET CENTRE<br>OF EXCELLENCE    | FSG<br>GEOTECHNICS<br>+FOUNDATION  |  | YOUR N<br>RESEAR                                       |





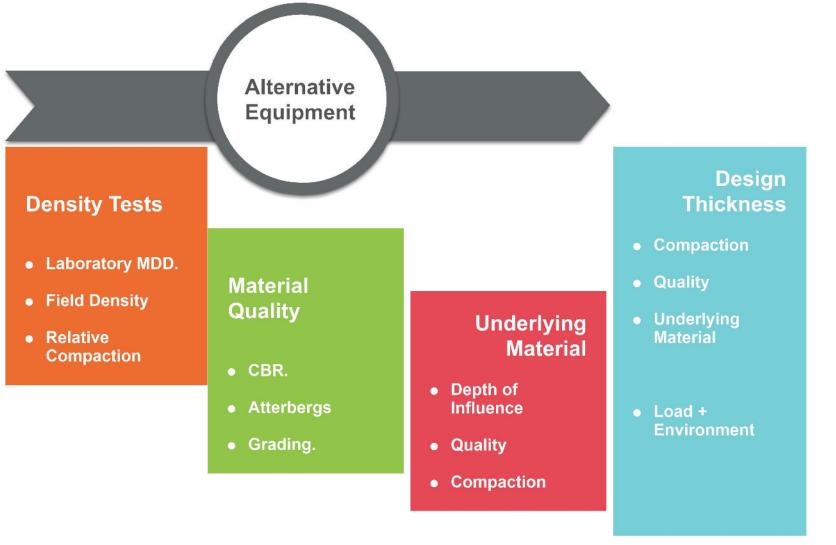
CBR

2.5 CBR

5

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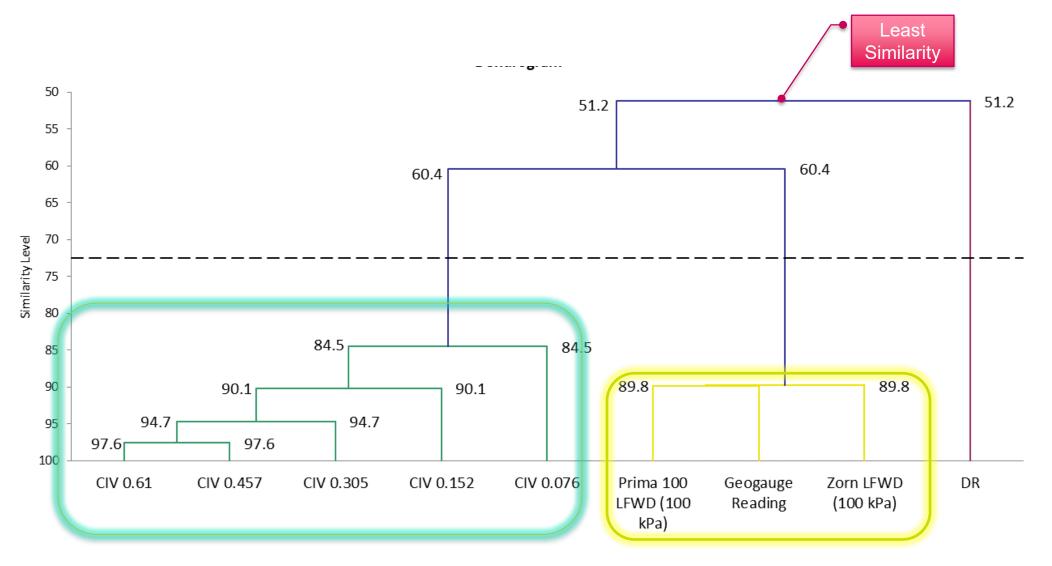
#### Comparison of Density vs alternative testing







### **Alternate Testing Dendograms**







#### Density Ratio is least correlated to the other 4

| Correlation              | DR    | Geogauge<br>Reading | Zorn LFWD<br>(100 kPa) | Prima LFWD<br>(100 kPa) | CIV<br>0.076 | CIV<br>0.152 | CIV<br>0.305 | CIV<br>0.457 | CIV 0.61 |
|--------------------------|-------|---------------------|------------------------|-------------------------|--------------|--------------|--------------|--------------|----------|
| DR                       | 1.00  |                     |                        |                         |              |              |              |              |          |
| Geogauge Reading         | -0.32 | 1.00                |                        |                         |              |              |              |              |          |
| Zorn LFWD (100 kPa)      | -0.23 | 0.79                | 1.00                   |                         |              |              |              |              |          |
| Prima 100 LFWD (100 kPa) | -0.30 | 0.77                | 0.81                   | 1.00                    |              |              |              |              |          |
| CIV 0.076                | 0.03  | 0.39                | 0.51                   | 0.30                    | 1.00         |              |              |              |          |
| CIV 0.152                | 0.10  | 0.24                | 0.40                   | 0.17                    | 0.79         | 1.00         |              |              |          |
| CIV 0.305                | 0.28  | -0.02               | 0.13                   | -0.11                   | 0.65         | 0.89         | 1.00         |              |          |
| CIV 0.457                | 0.35  | -0.01               | 0.10                   | -0.13                   | 0.62         | 0.83         | 0.94         | 1.00         |          |
| CIV 0.61                 | 0.31  | -0.06               | 0.10                   | -0.11                   | 0.62         | 0.83         | 0.93         | 0.95         | 1.00     |







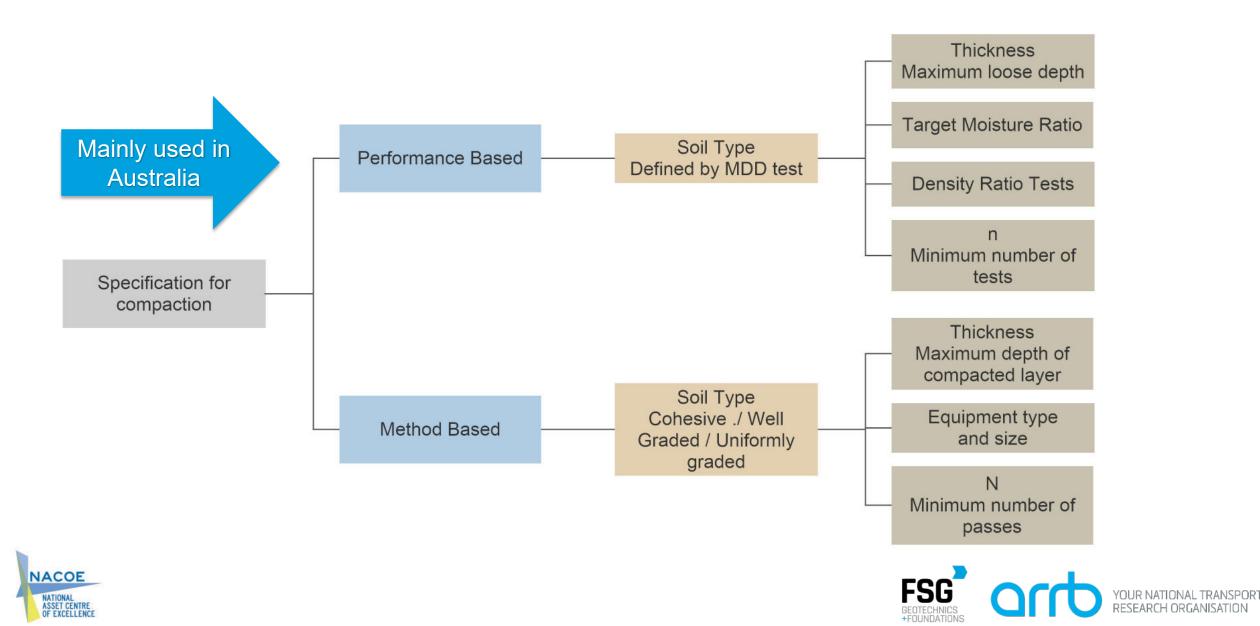
# Is Density Ratio the end game ?

. . . . . . . .





#### Performance based mainly used in Australia

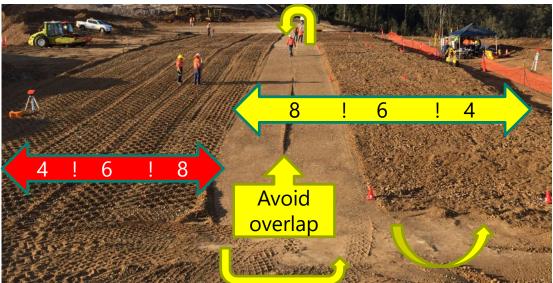


### Performance based uncertainty

#### Performance based specification used as it has more certainty – Does it? Pad Foot + Smooth Drum vibrating rollers





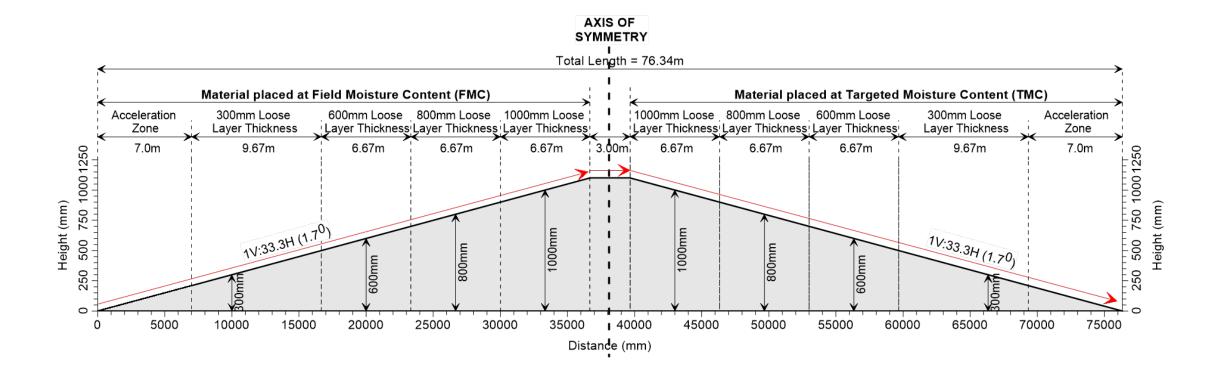








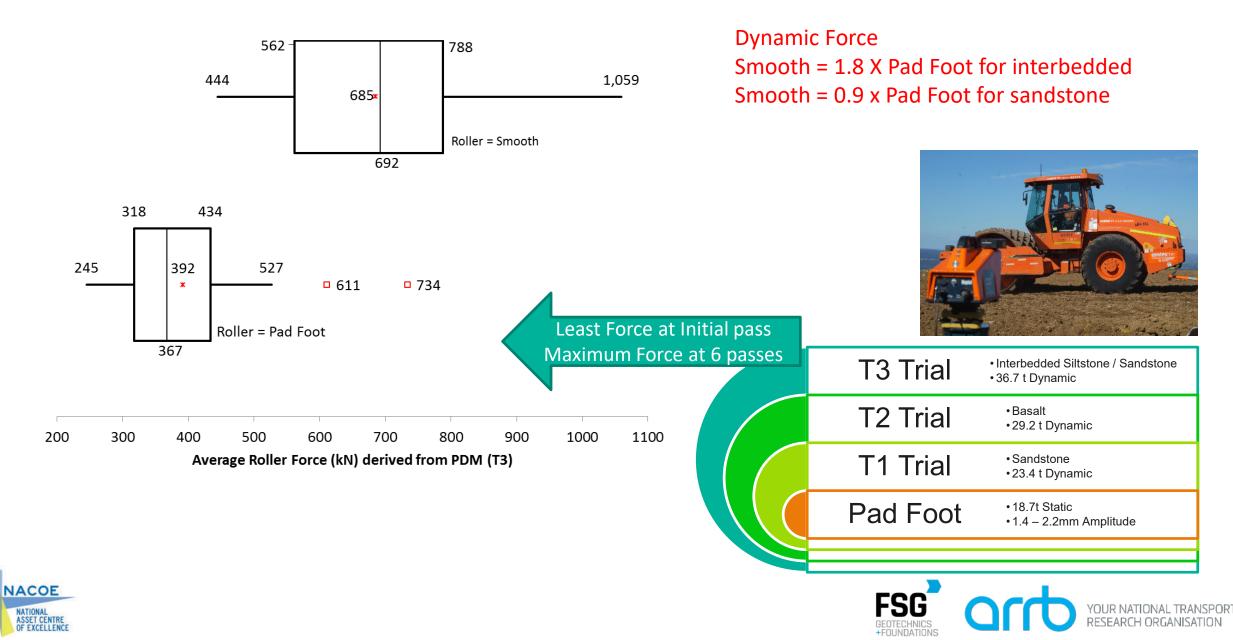
#### **Trial Embankment Layout Elevation**



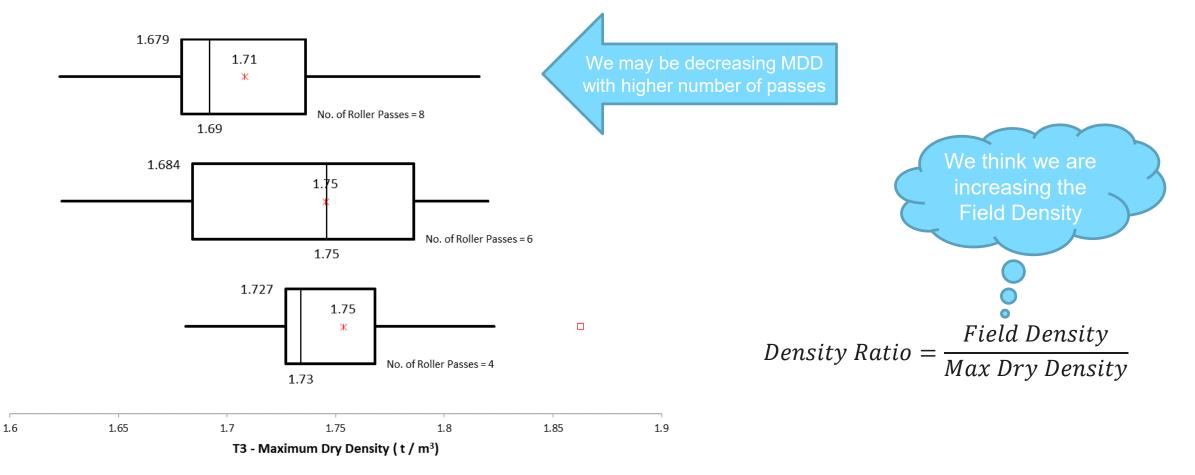




### **Dynamic Monitoring - Force**



#### Maximum Dry Density – T3 interbedded Siltstone / Sandstone







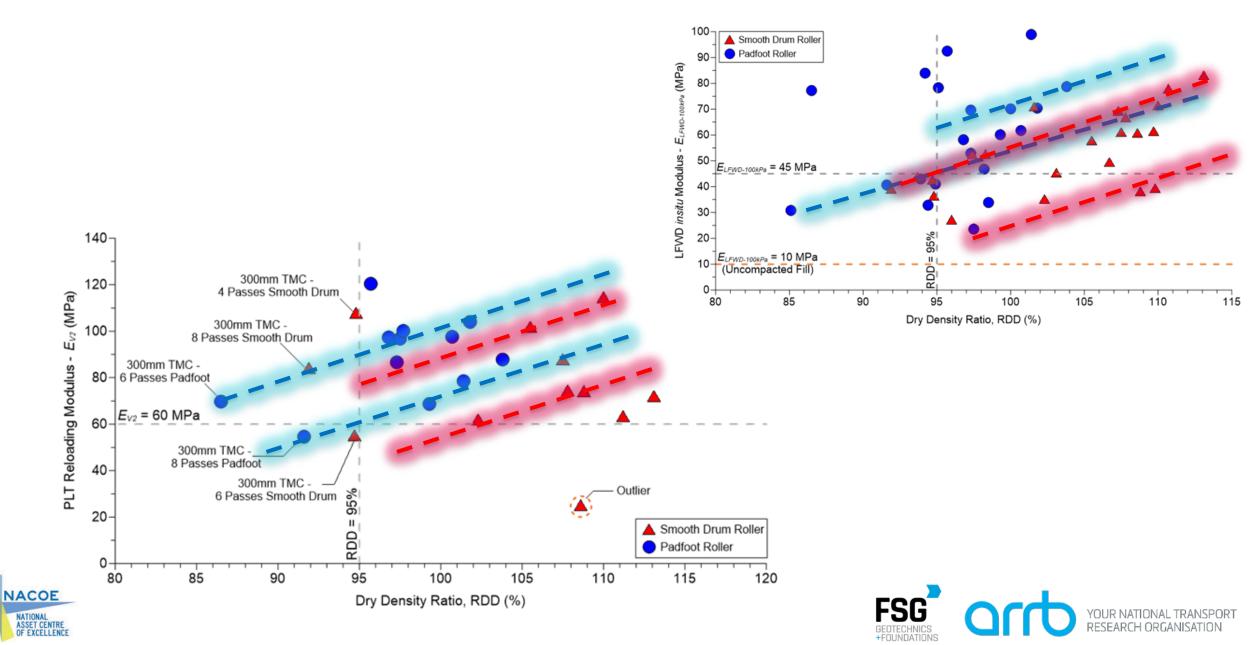
#### In situ E correlated to 95% Density ratio

| Fill Material Origin   | Plate Load Test<br>(PLT)<br>E <sub>v2</sub> (MPa) | Light Falling Weight Deflectometer<br>(LFWD)<br>E <sub>LFWD-100kPa</sub> (MPa) |
|--|---|--|
| Sandstone:<br>70% Gravel size; 10% fines                           | 60  | 45   |
| Interbedded Siltstone /<br>Sandstone<br>70% Gravel size; 11% fines | 35  | 25   |
| Basalt<br>65% Gravel size; 12% fines                               | 50  | 30   |





#### Modulus correlated to DR for sandstone material



#### These findings are not unique

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#### Modulus-Based Construction Specification for Compaction of Earthwork and Unbound Aggregate

#### DRAFT FINAL REPORT

Prepared for National Cooperative Highway Research Program NCHRP Project 10-84

> Transportation Research Board of The National Academics

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August 2014

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#### A Comparison of Density-Based and Modulus-Based In Situ Tests for Earthwork Quality Control

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**ABSTRACT:** A series of density-based and modulus-based quality control tests were performed to evaluate and compare the performance of a number of in situ testing methods for control of soil compaction. This paper highlights the results from the study that focus on three in situ testing tools for compaction control: the Light Weight Deflectometer (LWD), the Dynamic Cone Penetrometer (DCP), and the Nuclear Density Gauge (NDG). In situ tests conducted using these tools were performed during construction of an embankment built with a coarse-grained soil in a series of lifts. Comparison of the in situ test results shows that that there is a notable variability in measured soil properties for each of the testing methods that were performed. All three in situ tests showed an increasing trend in the measured properties for proper control of the compacton process. However, the soil moduli measured by the LWD and DCP correlated poorly to the NDG dry unit weights.

#### 9.2 General Conclusions

The general conclusions based on evaluation of the proposed modulus-based specification are the following:

- The adaption of the modulus-based specification needs to be approached in the context of the levels of uncertainty associated with the current well-established density criteria (especially when nuclear density gauges are used). It has been shown on many occasions in this study that achieving quality compaction (defined as achieving adequate layer modulus) is only weakly associated with achieving density.
- Among the modulus/stiffness-based technologies, devices based on the ultrasonic surface wave, lightweight deflectometer, and dynamic cone penetrometer technologies (PSPA, LWD, and DCP devices, respectively) perform reasonably well with the following caveats:
  - The PSPA exhibits the highest variability and needs the most training, but provides the most reasonable layer-specific information.
  - Different LWDs estimate different moduli at the same test spot. As such, the specification should be clear which LWD should be used. It is also important to consider the properties of the underlying layers in setting the LWD target values, especially when the layer of interest is overlying a layer with a significantly different modulus.
  - The DCP is simple to use and inexpensive. However, since DCP strictly measures the strength not the modulus of the layer, setting its target should be done with care. The DCP results were not very sensitive to moisture content and material changes.
- Among the modulus-based technologies evaluated, the LWD is recommended. This decision was
  partly made based on the familiarity of the highway agencies with the deflection concept, the ease of
  use of the device, and the availability of a network of providers of LWDs throughout the world.



### DR used to assess Strength or modulus

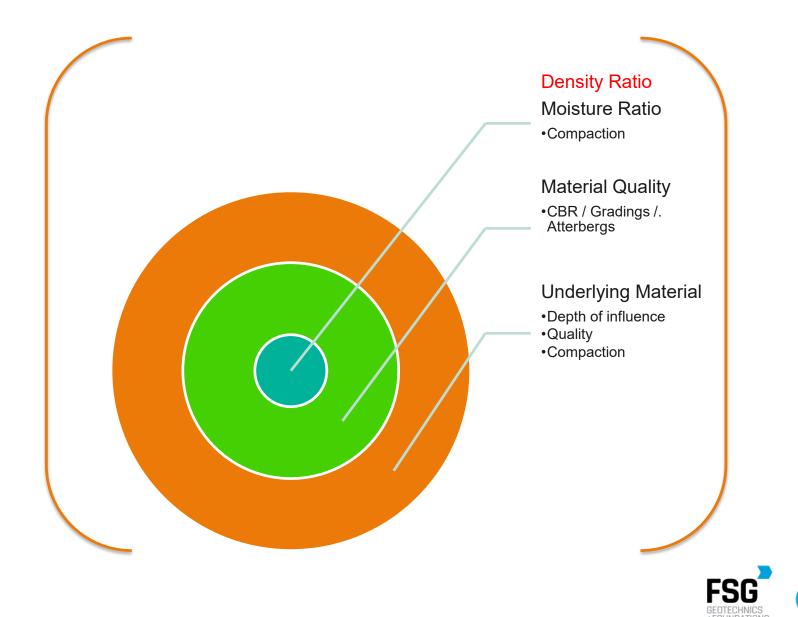
- $\checkmark~$  DR is currently the basis to assess quality during construction
- Prior to this research we assumed higher density was also a higher strength or modulus
- ✓ We were wrong

NACOE

- $\checkmark$  Correlating alternative testing to DR often results in a poor correlation
- $\checkmark\,$  Alternate testings generally correlate to each other
- ✓ These tests are combining DR + several other factors
- ✓ Modulus is more dependent on moisture rather than DR
- ✓ DR is a very precise test but may not be accurate



#### Multiple Targets measured: DR + Quality + Underlying interaction



Alternate Tests are measuring more than 1 variable

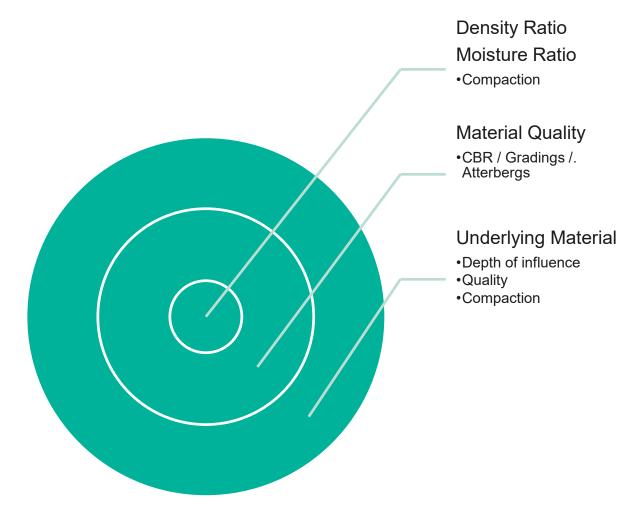
Partly accounts for the low R<sup>2</sup>

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#### Alternate Tests measure – One Target







# I DON'T ALWAYS KILL MY MAIN CHARACTERS BUT WHEN I DO... OK, YEAH. I ALWAYS DO

# Stay tuned for part 3





### Thank you for your participation today.

For further information on the topic, please contact:

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